June 28, 2019

Mr. Dana Valleau
Environmental Specialist
TRC Environmental Corporation
6 Ashley Drive
Scarborough, Maine 04074

Re: Chinook Solar PV Farm, Fitzwilliam, NH – Acoustic Study Report ***Ref. 4447***

Dear Dana:

This letter report presents the results of an acoustic study for the Chinook Solar PV Farm in Fitzwilliam, NH (herein referred to as the Project). The ground-based solar panels will cover an area of approximately 111 acres, within which equipment pads will house fifteen (15) inverters for converting Direct Current (DC) to Alternating Current (AC), and one substation with an 18/24 MVA power transformer to step-up the voltage of power delivered to the utility grid. The inverters will only operate in the daytime when electricity is produced by the solar panels. The substation will operate both during the daytime and nighttime. The acoustic study included both baseline sound monitoring and acoustic modeling. The acoustic modeling included 51 residential receptors surrounding the site. The results of the acoustic study were compared to the New Hampshire Site Evaluation Committee and the Town of Fitzwilliam noise ordinance incremental sound limits. The predicted change in sound levels would range from 0 to 6 dBA above the existing baseline ambient L_{90} daytime and nighttime sound levels and there would be no tonal sounds predicted at the residential receptors. Therefore, the Project will comply with both the New Hampshire Site Evaluation Committee and Town of Fitzwilliam noise ordinance incremental sound limits.

THE DECIBEL SCALE FOR SOUND

All sounds originate with a source – a human voice, vehicles on a roadway, or an airplane overhead. The sound energy moves from the source to a person's ears as sound waves, which are minute variations of air pressure. The loudness of a sound depends on the sound pressure level, which has units of decibel (dB). The decibel scale is logarithmic to accommodate the wide range of sound intensities to which the human ear is subjected. On this scale, the quietest sound we can hear is 0 dB, while the loudest is 120 dB. Every 10-dB increase is perceived as a doubling of loudness. Most sounds we hear in our daily lives have sound pressure levels in the range of 30 dB to 90 dB.

Community noise studies and regulations use an A-weighting scale (dBA) when measuring sound pressure levels as this approximates the response of the human ear to sounds, we experience in everyday life. Typical sound levels associated with various activities and environments are presented in **Figure 1**. Here are examples of sound levels we all encounter. A quiet suburban area at night without any traffic typically has an average sound level of 40 to 45 dBA. The freight train you hear in the distance may be 50 dBA, and crickets and tree frogs in the summer sing a sound level of 55 dBA. Two people having a

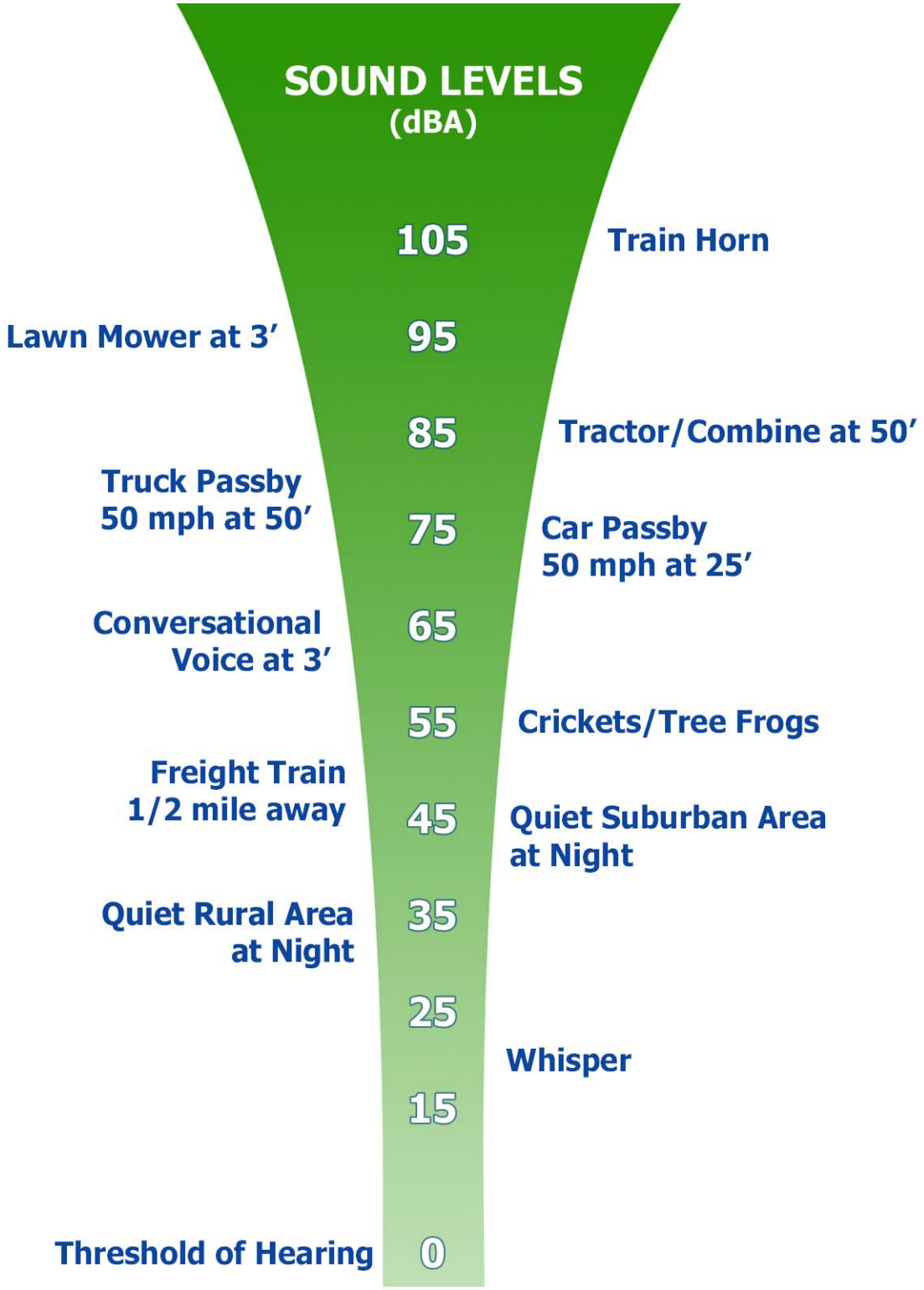

FIGURE 1.
Common Outdoor Sound Levels

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conversation in a normal tone of voice will hear each other speak at 65 dBA. Standing near a road, a car passing by can produce 75 dBA, and a truck passing by is louder at 80 dBA.

There are various measures of sound pressure designed for different purposes. To establish the background ambient sound level in an area, the L_{90} metric, which is the sound level exceeded 90 percent of the time, is typically used. The L_{90} can also be thought of as the level representing the quietest 10 percent of any time period. The L_{10} metric, which is the sound level exceeded 10 percent of the time is typically used to assess transient noise highway or rail activities. The L_{eq}, or equivalent sound level, is the steady-state sound level over a period of time that has the same acoustic energy as the fluctuating sounds that actually occurred during that same period. It is commonly referred to as the average sound level. The L_{max}, or maximum sound level, represents the one second peak level experienced during a given time period. These are a broadband sound pressure measure, i.e., it includes sounds at all frequencies.

Sound level measurements typically include an analysis of the sound spectrum into its various frequency components to determine tonal characteristics. The unit of frequency is Hertz (Hz), measuring the cycles per second of the sound pressure waves, and typically the frequency analysis examines eleven octave bands from 16 to 16,000 Hz.

APPLICABLE NOISE REGULATIONS

New Hampshire Site Evaluation Committee

The New Hampshire Site Evaluation Committee (NHSEC), Chapter Site 300 Certificates of Site and Facility, Part 301.08(d) for all energy facilities, except for wind energy facilities, requires that the SEC application include "an assessment of operational sound associated with the proposed facility, if the facility would involve use of equipment that might reasonably be expected to increase sound by 10 decibel A-weighted (dBA) or more over background levels, measured at the L_{90} sound level, at the property boundary of the proposed facility site or, in the case of an electric transmission line or an energy transmission pipeline, at the edge of the right-of-way or the edge of the property boundary if the proposed facility, or portion thereof, will be located on land owned, leased or otherwise controlled by the applicant or an affiliate of the applicant."

Town of Fitzwilliam

Under the Town of Fitzwilliam Zoning Code, Commercial and Industrial Noise – Chapter 130, the Town has established a maximum allowable incremental noise increases of 10 dBA above ambient. Daytime is defined as 7 AM to 10 PM and nighttime is defined as 10 PM to 7 AM. The Town sound limits are applicable to the L_{10} sound metric. The applicable daytime background one-hour L_{90} sound levels are 30 dBA for Rural Residential Districts and 38 dBA for Town Center; thus, the maximum allowable one-hour L_{10} noise limit is 40 dBA and 48 dBA respectively. The applicable nighttime background one-hour L_{90} sound levels are 24 dBA for Rural Residential Districts and 25 dBA for Town Center; thus, the maximum allowable one-hour L_{10} noise limit is 34 dBA and 35 dBA respectively.

These noise limits may also be lowered by up to 5 dBA if the source is producing either a tonal, low frequency or infrasound sounds. These penalties are cumulative up to a maximum of 10 dBA. The ordinance also allows for the developer to perform 24-hour baseline monitoring to establish the lowest daytime and nighttime ambient L_{90} values.

Since both the New Hampshire Site Evaluation Committee and Town of Fitzwilliam noise ordinance sound limits are based on ambient L_{90} baseline level + 10 dBA, ambient sound monitoring was performed for the Project.

AMBIENT SOUND MONITORING METHODS AND RESULTS

Tech set up a long-term sound analyzer to collect 24 hours of unattended ambient sound monitoring data. The analyzer was set up in the approximate center of the site. **Figure 2** shows the layout plan for the Project's solar panels, the nearby residences and the ambient monitoring location. The sound level measurements were collected using a Larson Davis 831 real-time sound level analyzer. The Larson Davis 831 is equipped with a ½" precision condenser microphone and has an operating range of 5 dB to 140 dB and an overall frequency range of 3.5 Hz to 20,000 Hz. The sound analyzer was mounted at an elevation of five feet with a windscreen. This ANSI Type 1 (high precision) sound analyzer was programmed to measure continuous real-time peak (L_{max}), average (L_{eq}), background level (L_{90}), higher transient levels (L_{10}), and one-third octave bands, measurements throughout the monitoring period. At the end of the monitoring period, Tech collected the sound analyzer and downloaded the data at our office for analysis.

Tech collected hourly sound measurements over a 24-hour period starting from 7 AM on Wednesday, May 8, 2019 and ending at 6 AM on Thursday, May 9, 2019. Weather conditions were favorable for ambient monitoring with clear skies, light winds (0-13 mph) and temperatures ranged from 34º to 63ºF.[1] As described above, the Fitzwilliam noise ordinance defines daytime as 7 AM to 10 PM and nighttime as 10 PM to 7 AM. The lowest daytime L_{90} sound level was 23 dBA, which was measured during the 9 PM hour. The lowest nighttime L_{90} sound level was 20 dBA, which was measured during the 12 AM hour. **Table 1** presents a summary of the hourly sound measurements. There were no tonal sounds measured during either quietest hour. Tech observed that the ambient sound conditions were dominated by motor vehicles along Highway 119 (NH-119) and Highway 12 (NH-25), and birds in the vicinity.

The lower measured ambient sound levels were used, instead of ambient sound levels in the Town of Fitzwilliam Noise Ordinance, in the acoustic modeling analysis to assess compliance with both the NHSEC and Fitzwilliam incremental sound limits.

PREDICTED PROJECT SOUND LEVELS

Future sound levels from the Chinook Solar PV Farm, when it is producing maximum electrical power, were calculated with the Cadna/A acoustic model. Cadna/A is a three-dimensional model for sound propagation and attenuation based on International Standard ISO 9613[2]. Atmospheric absorption, the process by which sound energy is absorbed by the air, was calculated using ANSI S1.26-1995.[3] Digital terrain data for the project areas were analyzed to obtain terrain heights. The model assumes the most-favorable sound propagation conditions, as occur under downwind conditions or during a ground-based temperature inversion on a clear night. Under these atmospheric conditions, sound travels further than if a person is upwind from a source and the atmosphere is well mixed, which would dampen the sound.

[1] Weather data from Jaffery, NH airport.

[2] International Standard, ISO 9613-2, Acoustics – Attenuation of Sound During Propagation Outdoors, -- Part 2 General Method of Calculation.

[3] American National Standards Institute, ANSI S1.26-1995, "American National Standard Method for the Calculation of the Absorption of Sound by the Atmosphere," 1995.

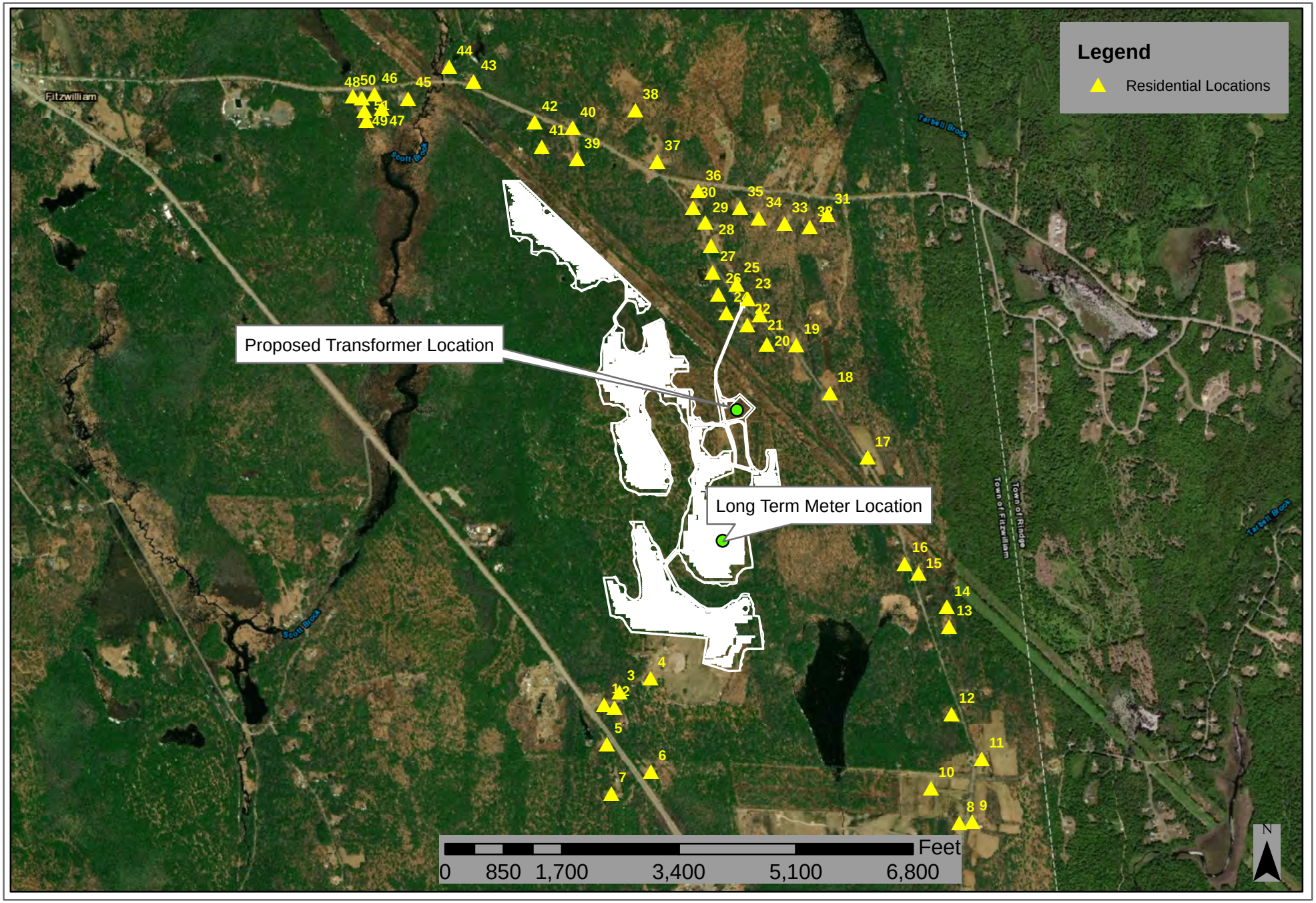

FIGURE 2.
Project Layout Plan
Chinook Solar PV Farm, Fitzwilliam, New Hampshire

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TABLE 1

AMBIENT SOUND LEVEL MEASUREMENTS
Wednesday, May 8 and Thursday, May 9, 2019

Date	Start Time	L_{90}	L_{eq}	L_{max}
Wednesday May 8	7:00 AM	33.2	40.5	57.7
	8:00 AM	31.8	39.0	58.8
	9:00 AM	33.9	43.4	66.9
	10:00 AM	34.7	38.7	51.3
	11:00 AM	33.6	44.6	59.3
	12:00 PM	35.1	45.9	69.9
	1:00 PM	35.3	42.8	61.3
	2:00 PM	35.5	42.2	57.3
	3:00 PM	36.7	41.8	55.5
	4:00 PM	35.7	40.5	51.3
	5:00 PM	33.0	38.5	54.4
	6:00 PM	31.4	36.4	56.1
	7:00 PM	26.4	34.3	52.2
	8:00 PM	24.9	31.7	52.0
	9:00 PM	**22.8***	27.5	40.3
	10:00 PM	21.5	24.4	35.4
	11:00 PM	20.5	25.1	43.6
Thursday May 9	12:00 AM	**20.0****	22.6	35.0
	1:00 AM	20.5	21.9	29.5
	2:00 AM	21.0	28.6	46.1
	3:00 AM	20.1	28.3	46.8
	4:00 AM	23.7	36.2	49.8
	5:00 AM	34.8	41.8	59.7
	6:00 AM	35.5	43.2	62.4

*Lowest daytime L_{90} level.
**Lowest nighttime L_{90} level.

The manufacturer's specification for the 920-KW inverters provided a sound pressure level of 75 dBA at 3 feet for the inverters, which is equivalent to a sound power level of 82 dBA[4,5]. This sound power level was used in Cadna/A for each inverter. The proposed transformer will be a 18/24 MVA unit with a projected National Electrical Manufacturers Association (NEMA) sound level rating of 75 dBA based on the maximum output of 24 MVA.[6] The sound power level of 93 dBA, used in Cadna/A, was

[4] The acoustic energy level of a source is known as its sound power level (L_w), which is also measured on a decibel scale. The sound power level of a source is the same at any distance; therefore, L_w values do not have reference distances.
[5] TMEIC Ninja PV-PCS 800-920-KW Inverter.
[6] Edison Electric Institute, Electric Power Plant Environmental Noise Guide, 1983, p. 4-17.

calculated based on the NEMA sound level rating and dimension of the proposed transformer.[7] The transformer will be located on the eastern side of the site adjacent to the existing electrical transmissions lines (See **Figure 2**). The modeling analysis assumes that both the inverters and transformer will operate at maximum load during the daytime. During the nighttime, the inverters do not operate and the transformer will operate at a lower load. However, it is conservatively assumed in the acoustic model that the transformer will operate at its maximum load at night.

Figure 2 shows the modeling receptors included in Cadna/A representing the 51 residential locations surrounding the site. The ambient L_{90} sound levels and the predicted daytime and nighttime sound levels for each residence are presented in **Table 2**. Decibel-level contour maps of the predicted Project daytime and nighttime sound levels are presented in **Figures 3 and 4** for daytime and nighttime, respectively. Attachment A presents the acoustic modeling results.

The predicted sound level increases range from 0 to 5 dBA above the existing baseline ambient L_{90} daytime sound levels and range from 0 to 6 above the existing baseline ambient L_{90} nighttime sound levels. The predicted sound levels for the receptors are based on the ambient sounds from the middle of the project site, which is further away from the surrounding roads. Therefore, the increases above ambient sounds at the receptors are likely conservative. Furthermore, there would be no tonal sounds predicted at the residential receptors. Therefore, the Project will comply with both the New Hampshire Site Evaluation Committee and Town of Fitzwilliam noise ordinance incremental sound limits.

CONCLUSIONS

An acoustic study was performed for the Chinook Solar PV Farm in Fitzwilliam, NH. The results of the acoustic study showed the operations of the fifteen (15) inverters and one substation with an 18/24 MVA power transformer will comply with the New Hampshire Site Evaluation Committee and Town Fitzwilliam noise ordinance sound limits.

Please call if you have any questions regarding this report.

Sincerely,

TECH ENVIRONMENTAL, INC.

Marc C. Wallace, QEP, INCE
Vice President
4447/Sound Report June 28 2019

[7] The NEMA sound level rating differs from the estimated sound power level that is used in sound source modeling. Tech Environmental used the NEMA sound level rating and dimensions of the transformer to calculate its anticipated sound power level. This calculation assumes that the NEMA sound level ratings includes the sound impacts of all associated cooling fans.

TABLE 2

PREDICTED SOUND LEVELS AT NEARBY RESIDENCES FROM THE CHINOOK SOLAR PROJECT AT PREDICTED SOUND LEVEL

Receptor ID	Residence Address	Predicted Sound Level (dBA)		Ambient Sound Level (dBA)		Total Predicted Sound Level (dBA)		Predicted Sound Level Increase (dBA)	
		Day	Night	Day	Night	Day	Night	Day	Night
1	10 Crane Road	17	10	23	20	24	20	1	0
2	3 Crane Road	17	10	23	20	24	20	1	0
3	19 Crane Road	17	11	23	20	24	21	1	1
4	35 Crane Road	20	12	23	20	24	21	2	1
5	532 Rt 12 S	15	9	23	20	24	20	1	0
6	549 Rt 12 S	14	9	23	20	23	20	1	0
7	550 Rt 12 S	14	8	23	20	23	20	1	0
8	444 Fullam Hill Road	11	6	23	20	23	20	0	0
9	423 Fullam Hill Road	10	6	23	20	23	20	0	0
10	414 Fullam Hill Road	12	7	23	20	23	20	0	0
11	391 Fullam Hill Road	12	7	23	20	23	20	0	0
12	364 Fullam Hill Road	14	9	23	20	23	20	1	0
13	309 Fullam Hill Road	15	11	23	20	24	21	1	1
14	307 Fullam Hill Road	16	11	23	20	24	21	1	1
15	277 Fullam Hill Road	16	13	23	20	24	21	1	1
16	264 Fullam Hill Road	17	14	23	20	24	21	1	1
17	199 Fullam Hill Road	21	19	23	20	25	23	2	3
18	161 Fullam Hill Road	24	22	23	20	26	24	3	4
19	123 Fullam Hill Road	24	23	23	20	26	25	4	5
20	106 Fullam Hill Road	26	25	23	20	27	26	5	**6**
21	99 Fullam Hill Road	23	22	23	20	26	24	3	4
22	94 Fullam Hill Road	25	23	23	20	27	25	4	5
23	85 Fullam Hill Road	23	21	23	20	26	23	3	3
24	88 Fullam Hill Road	24	22	23	20	27	24	4	4
25	73 Fullam Hill Road	22	20	23	20	25	23	3	3
26	68 Fullam Hill Road	23	21	23	20	26	23	3	3

TABLE 2 (CONT.)

PREDICTED SOUND LEVELS AT NEARBY RESIDENCES FROM THE CHINOOK SOLAR PROJECT AT PREDICTED SOUND LEVEL

Receptor ID	Residence Address	Predicted Sound Level (dBA)		Ambient Sound Level (dBA)		Total Predicted Sound Level (dBA)		Predicted Sound Level Increase (dBA)	
		Day	Night	Day	Night	Day	Night	Day	Night
27	64 Fullam Hill Road	22	19	23	20	25	22	3	2
28	45 Fullam Hill Road	21	17	23	20	25	22	2	2
29	33 Fullam Hill Road	20	16	23	20	24	21	2	1
30	23 Fullam Hill Road	19	15	23	20	24	21	2	1
31	484 RT 119 E	16	14	23	20	24	21	1	1
32	468 RT 119 E	17	15	23	20	24	21	1	1
33	462 RT 119 E	17	16	23	20	24	21	1	1
34	450 RT 119 E	18	16	23	20	24	21	1	1
35	432 RT 119 E	18	15	23	20	24	21	1	1
36	406 RT 1119 E	18	14	23	20	24	21	1	1
37	377 RT 1119 E	18	12	23	20	24	21	1	1
38	347 RT 1119 E	16	10	23	20	24	20	1	0
39	334 RT 119 E	21	11	23	20	25	21	2	1
40	327 RT 119 E	17	10	23	20	24	20	1	0
41	328 RT 119 E	19	10	23	20	24	20	1	0
42	310 RT 119 E	17	9	23	20	24	20	1	0
43	269 RT 1119 E	13	7	23	20	23	20	0	0
44	253 RT 1119 E	13	6	23	20	23	20	0	0
45	224 RT 1119 E	13	6	23	20	23	20	0	0
46	6 Phillips CT	12	6	23	20	23	20	0	0
47	14 Phillips CT	13	6	23	20	23	20	0	0
48	206 RT 1119 E	12	5	23	20	23	20	0	0
49	15 Doyle CT	12	6	23	20	23	20	0	0
50	5 Doyle CT	12	5	23	20	23	20	0	0
51	18 Doyle CT	12	6	23	20	23	20	0	0

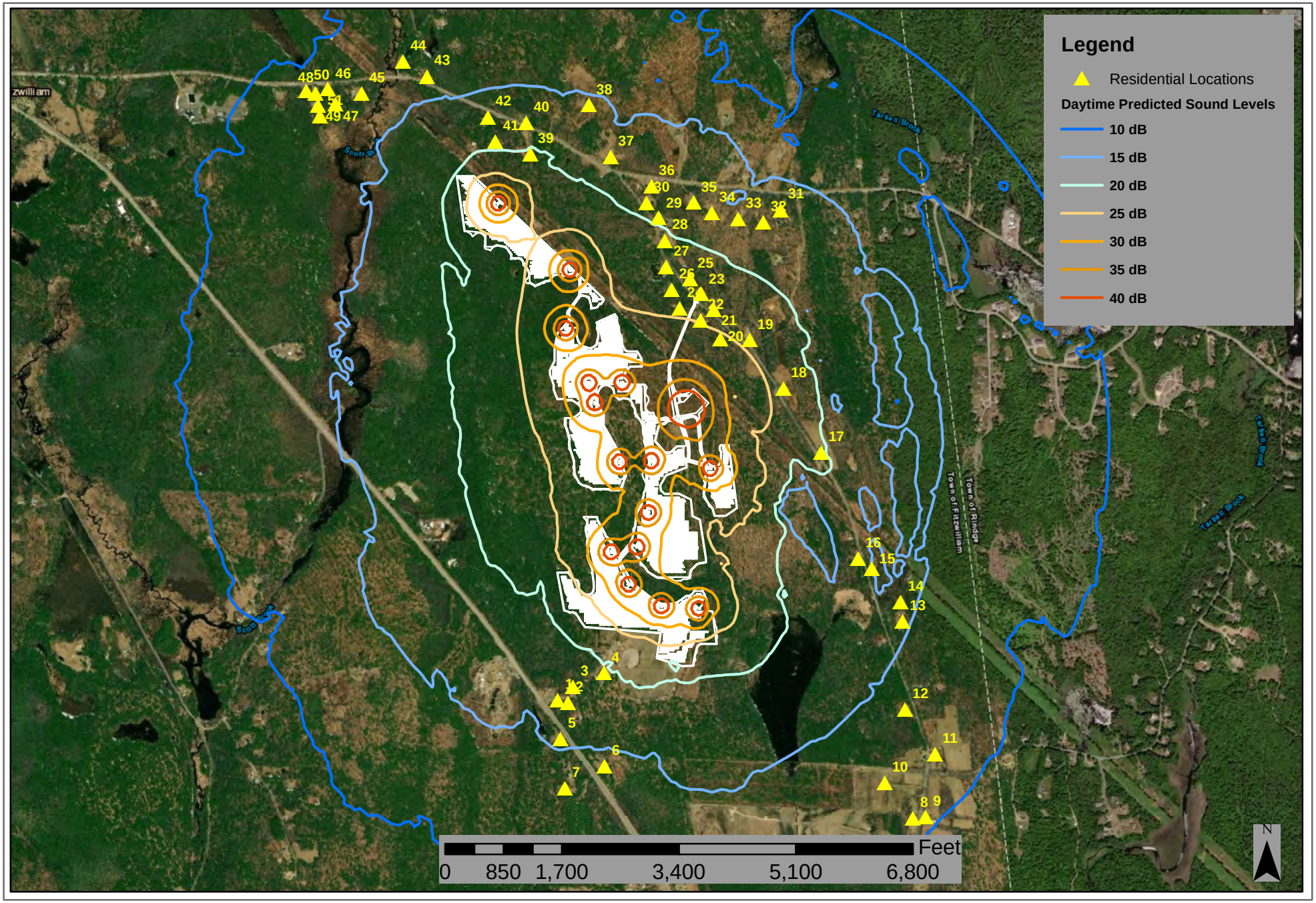

FIGURE 3.
Daytime Predicted Sound Levels
Chinook Solar PV Farm, Fitzwilliam, New Hampshire

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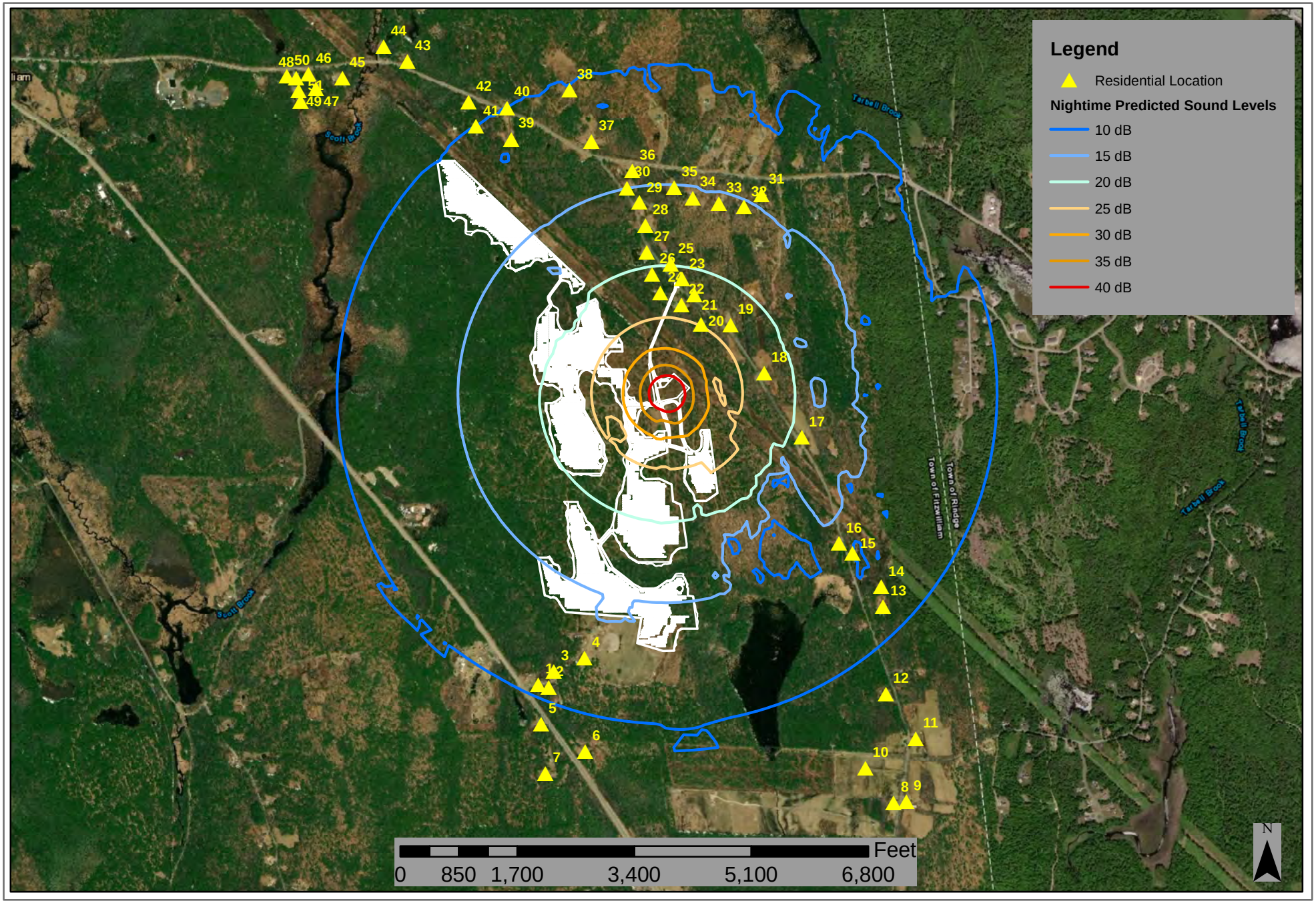

FIGURE 4.
Nighttime Predicted Sound Levels
Chinook Solar PV Farm, Fitzwilliam, New Hampshire

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ATTACHMENT A

ACOUSTIC MODELING RESULTS

Daytime Octave Band Analysis

Receptor ID	Address	Octave Band L90 (dB) from Source																										
		25.0	31.5	40.0	50.0	63.0	80.0	100	125	160	200	250	315	400	500	630	800	1000	1250	1600	2000	2500	3150	4000	5000	6300	8000	10000
1	10 Crane Road	-49.0	-40.7	-25	-33.6	-29.7	-20.2	-12.8	3	-10.5	-7.7	5.3	3.9	11.2	11.3	7.1	4.9	0.7	-3	-7.6	-13.3	-19.5	-27.6	-39.5	-54.5	-73.4	-81.3	-82.7
2	3 Crane Road	-48.9	-40.6	-24.9	-33.6	-29.7	-20.1	-12.7	3.1	-10.5	-7.6	5.4	4	11.3	11.4	7.2	5	0.8	-2.9	-7.5	-13.1	-19.2	-27.2	-38.9	-53.7	-72.5	-81.3	-82.7
3	19 Crane Road	-48.2	-39.9	-24.2	-32.9	-29	-19.4	-11.9	3.9	-9.7	-6.8	6.1	4.8	12	12.2	8	5.7	1.7	-2	-6.4	-11.9	-17.7	-25.2	-36.2	-49.8	-67.4	-81	-82.7
4	35 Crane Road	-46.6	-38.4	-22.6	-31.3	-27.4	-17.8	-10	5.8	-7.7	-5.1	8	6.7	14.1	14.4	10.3	8.1	4.2	0.8	-3.3	-8.2	-13.1	-19.5	-28.9	-40.3	-54.8	-74	-82.7
5	532 Rt 12 S	-49.3	-41	-25.2	-33.9	-30	-20.4	-14.1	1.7	-11.9	-9	3.9	2.6	10	10.2	5.9	3.8	-0.4	-4.3	-9.1	-15.2	-21.9	-30.9	-44.1	-61.2	-78.9	-81.3	-82.7
6	549 Rt 12 S	-50.6	-42.4	-26.6	-35.3	-31.4	-21.8	-14.7	1.1	-12.5	-9.5	3.5	2.1	9.1	9.2	4.9	2.5	-1.8	-5.9	-10.9	-17.4	-24.6	-34.2	-48.1	-65.8	-79.9	-81.3	-82.7
7	550 Rt 12 S	-51.5	-43.3	-27.5	-36.2	-32.2	-22.6	-15.7	0.1	-13.5	-10.6	2.4	1	8.5	8.7	4.4	2	-2.4	-6.5	-11.6	-18.1	-25.6	-35.8	-50.9	-70.6	-80.3	-81.3	-82.7
8	444 Fullam Hill Road	-51	-42.7	-26.9	-35.6	-31.7	-22.1	-18.6	-2.8	-16.5	-13.6	-0.8	-2.3	5.5	5.5	1.1	-0.4	-5	-9.6	-15.2	-23.1	-32.6	-46	-65.7	-79.5	-80.3	-81.3	-82.7
9	423 Fullam Hill Road	-54.2	-45.9	-30.1	-38.8	-34.9	-25.3	-18.7	-3	-16.6	-13.7	-0.9	-2.4	5.3	5.3	0.8	-1.4	-5.8	-10.4	-16.3	-24.1	-33.7	-47.4	-67.4	-79.6	-80.3	-81.3	-82.7
10	414 Fullam Hill Road	-48.4	-40.1	-24.3	-32.9	-29	-19.4	-17.5	-1.8	-15.4	-12.4	0.4	-1	6.9	7	2.6	2.2	-2.2	-6.4	-11.3	-18.1	-26.1	-37.2	-53.8	-74.8	-80.3	-81.3	-82.7
11	391 Fullam Hill Road	-48	-39.7	-23.9	-32.6	-28.6	-19	-17.8	-2.1	-15.7	-12.8	0.1	-1.4	6.6	6.6	2.2	2.1	-2.3	-6.6	-11.6	-18.7	-27.3	-39.3	-57.3	-77.7	-80.3	-81.3	-82.7
12	364 Fullam Hill Road	-46.6	-38.3	-22.6	-31.2	-27.3	-17.6	-16.5	-0.7	-14.3	-11.4	1.5	0.1	8.2	8.3	4	4	-0.2	-4.2	-8.8	-15.3	-22.8	-33.2	-48.8	-69.3	-80.3	-81.3	-82.7
13	309 Fullam Hill Road	-46.1	-37.9	-22.1	-30.7	-26.8	-17.1	-15	0.9	-12.6	-9.8	3.2	1.8	9.7	9.9	5.7	5.4	1.3	-2.6	-7	-13.1	-20	-29.6	-44	-62.9	-79.8	-81.3	-82.7
14	307 Fullam Hill Road	-46	-37.7	-21.9	-30.5	-26.6	-17	-14.6	1.2	-12.3	-9.4	3.6	2.2	10	10.1	5.9	5.6	1.5	-2.3	-6.7	-12.7	-19.6	-29.2	-43.5	-62.3	-79.7	-81.3	-82.7
15	277 Fullam Hill Road	-49.2	-40.9	-25.2	-33.8	-29.9	-20.3	-13.3	2.5	-11	-8.1	4.8	3.4	10.8	11	6.8	4.9	0.8	-2.9	-7.5	-13.3	-19.8	-28.7	-41.7	-58.1	-77.3	-81.3	-82.7
16	264 Fullam Hill Road	-48.6	-40.4	-24.7	-33.3	-29.4	-19.9	-12.6	3.2	-10.4	-7.6	5.3	4	11.2	11.4	7.3	5.2	1.1	-2.6	-7.1	-12.9	-19.3	-28.1	-41.2	-57.8	-77	-81.3	-82.7
17	199 Fullam Hill Road	-45.5	-37.2	-21.4	-30	-26.1	-16.4	-8.3	7.6	-5.8	-4.3	8.8	7.6	15.2	15.6	11.5	10.2	6.5	3.3	-0.5	-5.2	-10	-16.5	-26.6	-39.6	-57	-78.8	-82.7
18	161 Fullam Hill Road	-43.1	-34.8	-19	-27.7	-23.7	-14	-5.8	10.2	-3.2	-2	11.2	10.1	17.9	18.3	14.4	13.3	9.7	6.7	3.3	-0.9	-4.9	-10.2	-18.4	-28.5	-41.7	-61.1	-81.8
19	123 Fullam Hill Road	-42.7	-34.5	-18.7	-27.3	-23.3	-13.6	-5.4	10.6	-2.8	-1.6	11.6	10.5	18.2	18.6	14.7	13.6	10	7	3.6	-0.6	-4.5	-9.7	-17.6	-27.5	-40.2	-58.8	-80.8
20	106 Fullam Hill Road	-41.2	-32.9	-17.1	-25.7	-21.8	-12.1	-3.8	12.1	-1.2	0	13.2	12.1	19.8	20.2	16.4	15.4	11.8	9	5.7	1.8	-1.8	-6.5	-13.6	-22.2	-33	-48.7	-70.8
21	99 Fullam Hill Road	-43.2	-35	-19.2	-27.8	-23.8	-14.2	-5.9	10	-3.4	-2	11.2	10	17.6	18	14.1	12.9	9.2	6.2	2.7	-1.6	-5.7	-11.2	-19.6	-30.2	-43.9	-64.1	-82.3
22	94 Fullam Hill Road	-42.1	-33.9	-18.1	-26.7	-22.7	-13	-4.8	11.2	-2.2	-0.9	12.3	11.1	18.9	19.3	15.4	14.3	10.7	7.8	4.4	0.3	-3.5	-8.5	-16.3	-25.7	-37.9	-55.7	-78.8
23	85 Fullam Hill Road	-44	-35.7	-19.9	-28.5	-24.6	-14.9	-6.7	9.2	-4.2	-2.8	10.4	9.2	16.8	17.2	13.2	11.9	8.2	5.1	1.5	-3	-7.4	-13.3	-22.4	-33.9	-49.3	-71.4	-82.7
24	88 Fullam Hill Road	-42.7	-34.4	-18.6	-27.2	-23.3	-13.6	-5.3	10.6	-2.8	-1.4	11.7	10.6	18.4	18.9	14.9	13.8	10.2	7.2	3.7	-0.4	-4.4	-9.7	-17.9	-28	-41.2	-60.5	-81.6
25	73 Fullam Hill Road	-44.6	-36.3	-20.6	-29.2	-25.2	-15.6	-7.4	8.5	-4.9	-3.4	9.7	8.6	16.2	16.6	12.6	11.1	7.4	4.2	0.4	-4.2	-8.9	-15.3	-25.1	-37.7	-54.6	-77.3	-82.7
26	68 Fullam Hill Road	-43.8	-35.5	-19.7	-28.3	-24.4	-14.7	-6.5	9.5	-3.9	-2.5	10.6	9.5	17.4	17.8	13.8	12.4	8.7	5.7	2	-2.4	-6.8	-12.8	-22	-33.6	-49	-70.9	-82.7
27	64 Fullam Hill Road	-44.9	-36.6	-20.8	-29.4	-25.5	-15.8	-7.6	8.3	-5.1	-3.6	9.5	8.3	16.3	16.7	12.7	11.1	7.4	4.2	0.4	-4.2	-8.9	-15.3	-25	-37	-52.2	-72.2	-82.7
28	45 Fullam Hill Road	-46.1	-37.8	-22	-30.6	-26.6	-17	-9.1	6.9	-6.6	-4.8	8.3	7.1	15	15.4	11.4	9.7	5.9	2.6	-1.3	-6.2	-11.2	-18	-28	-40	-54.6	-74	-82.7
29	33 Fullam Hill Road	-46.9	-38.6	-22.8	-31.5	-27.5	-17.9	-10.2	5.7	-7.8	-5.7	7.4	6.2	14.1	14.5	10.4	8.6	4.8	1.5	-2.6	-7.6	-12.8	-19.6	-29.6	-41.2	-55.6	-75	-82.7
30	23 Fullam Hill Road	-47.3	-39	-23.3	-31.9	-27.9	-18.3	-10.7	5.1	-8.3	-6.1	7	5.7	13.7	14	10	8.1	4.2	0.9	-3.2	-8.3	-13.5	-20.4	-30.3	-41.8	-56.2	-75.5	-82.7
31	484 RT 119 E	-49.3	-41	-25.3	-34	-30.1	-20.5	-13.4	2.4	-11.1	-8.4	4.6	3.2	10.2	10.3	6.1	4.2	0	-3.9	-8.6	-14.6	-21.3	-30.9	-45.5	-65.3	-80.1	-81.3	-82.7
32	468 RT 119 E	-48.4	-40.2	-24.4	-33.1	-29.1	-19.5	-12.3	3.6	-9.9	-7.4	5.6	4.3	11.5	11.7	7.5	6	2	-1.6	-6.1	-11.6	-17.8	-26.5	-39.9	-58	-78.6	-81.3	-82.7
33	462 RT 119 E	-48.2	-39.9	-24.1	-32.8	-28.9	-19.3	-12	3.9	-9.7	-7.1	5.9	4.5	11.7	12	7.8	6.2	2.2	-1.3	-5.7	-11.2	-17.3	-25.8	-38.9	-56.7	-77.9	-81.3	-82.7
34	450 RT 119 E	-47.9	-39.6	-23.8	-32.5	-28.6	-19	-11.6	4.3	-9.2	-6.7	6.3	5	12.2	12.5	8.3	6.6	2.6	-1	-5.4	-10.9	-17	-25.5	-38.7	-56.4	-77.7	-81.3	-82.7
35	432 RT 119 E	-48	-39.7	-23.9	-32.6	-28.6	-19	-11.7	4.2	-9.3	-6.8	6.2	5	12.4	12.7	8.5	6.7	2.7	-0.9	-5.4	-11	-17.2	-25.9	-39.3	-57	-77.3	-81.3	-82.7
36	406 RT 1119 E	-48	-39.7	-24	-32.6	-28.6	-19	-11.6	4.3	-9.2	-6.9	6.2	4.9	12.9	13.1	9.1	7.2	3.3	-0.2	-4.4	-9.7	-15.3	-22.7	-33.4	-46.2	-62.4	-80	-82.7
37	377 RT 1119 E	-48.7	-40.4	-24.6	-33.2	-29.3	-19.7	-12.3	3.6	-9.9	-7.5	5.5	4.3	12.2	12.5	8.5	6.5	2.6	-0.9	-5	-10.1	-15.2	-21.7	-31.3	-43.2	-58.9	-78.7	-82.7
38	347 RT 1119 E	-50.3	-42.1	-26.3	-34.9	-31	-21.4	-14.1	1.7	-11.8	-9.3	3.7	2.4	10.2	10.5	6.3	4.1	0	-3.6	-8.1	-13.6	-19.2	-26.4	-36.9	-50.1	-67.5	-81.1	-82.7
39	334 RT 119 E	-40.7	-32.4	-16.6	-25.2	-21.2	-11.6	-8.3	7.7	-5.7	-5.9	7.2	6	14.6	15	11.1	12.5	9	6.2	3.5	-0.2	-3.4	-7.4	-13.6	-20.7	-29.3	-41.7	-59.2
40	327 RT 119 E	-49.3	-41	-25.2	-33.9	-29.9	-20.3	-12.7	3.2	-10.2	-8.1	5	3.8	12	12.3	8.4	6.2	2.5	-0.5	-3.9	-7.7	-10.9	-14.5	-21.9	-31	-42.7	-59.8	-80.4
41	328 RT 119 E	-48.1	-39.8	-24	-32.6	-28.7	-19	-11.3	4.6	-8.8	-6.7	6.4	5.2	13.4	13.8	9.9	7.8	4.1	1.1	-2.4	-6.4	-9.8	-14.1	-20.5	-27.8	-36.8	-49.7	-68
42	310 RT 119 E	-49.8	-41.5	-25.7	-34.3	-30.4	-20.8	-13.3	2.6	-10.8	-8.6	4.5	3.3	11.3	11.6	7.6	5.4	1.5	-1.8	-5.6	-10.1	-14.2	-19.4	-27	-36.3	-48.2	-65.5	-82
43	269 RT 1119 E	-52.3	-44	-28.2	-36.9	-32.9	-23.3	-16.2	-0.4	-13.9	-11.4	1.5	0.1	8	8.2	4	1.7	-2.4	-6.1	-10.6	-15.9	-21.2	-28	-38.2	-51.4	-68.9	-81.2	-82.7
44	253 RT 1119 E	-48.3	-40	-24.3	-32.9	-28.9	-19.3	-17.2	-1.4	-14.9	-12.3	0.6	-0.8	7.2	7.3	3.1	3.2	-0.9	-4.6	-8.5	-13.8	-19.5	-27.2	-39	-54.7	-75	-81.3	-82.7
45	224 RT 1119 E	-46.2	-37.9	-22.1	-30.7	-26.8	-17.2	-17.3	-1.5	-15.1	-12.4	0.5	-0.9	7.3	7.4	3.1	4.1	0	-3.8	-7.9	-13.6	-19.6	-27.6	-39.8	-55.9	-76.2	-81.3	-82.7
46	6 Phillips CT	-46.5	-38.2	-22.5	-31.1	-27.2	-17.5	-18.2	-2.4	-16	-13.2	-0.3	-1.8	6.4	6.4	2.1	3.1	-1.2	-5.2	-9.6	-15.8	-22.6	-31.7	-45.4	-63.8	-79.9	-81.3	-82.7
47	14 Phillips CT	-46.1	-37.8	-22	-30.6	-26.7	-17.1	-17.7	-1.9	-15.5	-12.8	0.1	-1.3	6.9	7	2.7	3.8	-0.4	-4.4	-8.6	-14.6	-21.1	-29.8	-42.7	-60	-78.8	-81.3	-82.7
48	206 RT 1119 E	-46.7	-38.4	-22.7	-31.3	-27.4	-17.8	-18.3	-2.6	-16.2	-13.4	-0.5	-2	6.2	6.2	1.8	2.8	-1.5	-5.6	-10.1	-16.4	-23.4	-32.8	-47	-65.9	-80.1	-81.3	-82.7
49	15 Doyle CT	-46.4	-38.2	-22.4	-31	-27.1	-17.5	-18.1	-2.3	-15.9	-13.1	-0.2	-1.7	6.5	6.5	2.2	3.2	-1.1	-5.1	-9.5	-15.7	-22.5	-31.7	-45.4	-63.7	-79.8	-81.3	-82.7
50	5 Doyle CT	-47	-38.7	-22.9	-31.5	-27.6	-18	-18.6	-2.8	-16.4	-13.6	-0.8	-2.3	5.9	5.9	1.5	2.5	-1.9	-6	-10.6	-17.1	-24.3	-34	-48.6	-68.1	-80.2	-81.3	-82.7
51	18 Doyle CT	-46.2	-37.9	-22.2	-30.8	-26.9	-17.3	-17.9	-2.1	-15.7	-12.9	0	-1.5	6.7	6.8	2.5	3.5	-0.7	-4.7	-9	-15.1	-21.8	-30.8	-44.2	-62	-79.5	-81.3	-82.7

	Octave Band L90 (dB) from Background																											
	25.0	31.5	40.0	50.0	63.0	80.0	100	125	160	200	250	315	400	500	630	800	1000	1250	1600	2000	2500	3150	4000	5000	6300	8000	10000
Lowest Day L90	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.6	16.9	18.2	19.0	17.2	15.2	14.0	14.4	13.5	10.6	6.7	4.6	3.7	3.8	4.6	5.3	6.3	7.2	7.9	8.4

Receptor ID	Address	Octave Band L90 (dB) from Source& Background																										
		25.0	31.5	40.0	50.0	63.0	80.0	100	125	160	200	250	315	400	500	630	800	1000	1250	1600	2000	2500	3150	4000	5000	6300	8000	10000
1	10 Crane Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.2	17.4	16.7	15.9	15.1	14.1	11.0	7.1	4.9	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
2	3 Crane Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.2	17.4	16.7	15.9	15.2	14.1	11.0	7.2	4.9	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
3	19 Crane Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.2	17.4	16.9	16.2	15.3	14.2	11.1	7.2	4.9	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
4	35 Crane Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.8	16.9	18.2	19.3	17.6	17.7	17.2	15.8	14.6	11.5	7.7	5.3	4.0	3.9	4.6	5.3	6.3	7.2	7.9	8.4
5	532 Rt 12 S	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.1	17.3	16.3	15.5	15.0	13.9	10.9	7.0	4.8	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
6	549 Rt 12 S	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.1	17.3	16.2	15.2	14.9	13.8	10.8	6.9	4.7	3.7	3.8	4.6	5.3	6.3	7.2	7.9	8.4
7	550 Rt 12 S	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.1	17.3	16.0	15.1	14.8	13.8	10.8	6.9	4.7	3.7	3.8	4.6	5.3	6.3	7.2	7.9	8.4
8	444 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.6	16.9	18.2	19.0	17.2	15.6	14.6	14.6	13.7	10.7	6.8	4.6	3.7	3.8	4.6	5.3	6.3	7.2	7.9	8.4
9	423 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.6	16.9	18.2	19.0	17.2	15.6	14.5	14.6	13.6	10.7	6.8	4.6	3.7	3.8	4.6	5.3	6.3	7.2	7.9	8.4
10	414 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.6	16.9	18.2	19.1	17.3	15.8	14.8	14.7	13.8	10.8	6.9	4.7	3.7	3.8	4.6	5.3	6.3	7.2	7.9	8.4
11	391 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.6	16.9	18.2	19.1	17.3	15.8	14.7	14.7	13.8	10.8	6.9	4.7	3.7	3.8	4.6	5.3	6.3	7.2	7.9	8.4
12	364 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.1	17.3	16.0	15.0	14.8	14.0	10.9	7.0	4.8	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
13	309 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.1	17.3	16.3	15.4	14.9	14.1	11.1	7.2	4.9	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
14	307 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.1	17.3	16.3	15.5	15.0	14.2	11.1	7.2	4.9	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
15	277 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.2	17.4	16.5	15.8	15.1	14.1	11.0	7.2	4.9	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
16	264 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.2	17.4	16.7	15.9	15.2	14.1	11.1	7.2	4.9	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
17	199 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.9	16.9	18.2	19.4	17.7	18.2	17.9	16.2	15.2	12.0	8.3	5.8	4.2	4.0	4.6	5.3	6.3	7.2	7.9	8.4
18	161 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	19.2	16.9	18.2	19.7	18.0	19.8	19.7	17.4	16.4	13.2	9.7	7.0	5.0	4.3	4.7	5.3	6.3	7.2	7.9	8.4
19	123 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	19.2	16.9	18.2	19.7	18.0	20.0	19.9	17.6	16.6	13.3	9.9	7.1	5.1	4.4	4.8	5.3	6.3	7.2	7.9	8.4
20	106 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	19.5	17.0	18.3	20.0	18.4	21.1	21.1	18.5	17.6	14.3	11.0	8.2	5.9	4.9	4.9	5.4	6.3	7.2	7.9	8.4
21	99 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	19.2	16.9	18.2	19.7	18.0	19.6	19.5	17.3	16.2	13.0	9.5	6.8	4.8	4.3	4.7	5.3	6.3	7.2	7.9	8.4
22	94 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	19.3	17.0	18.3	19.8	18.2	20.4	20.4	17.9	16.9	13.7	10.3	7.5	5.3	4.5	4.8	5.3	6.3	7.2	7.9	8.4
23	85 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	19.1	16.9	18.2	19.6	17.8	19.1	18.9	16.9	15.8	12.6	9.0	6.3	4.5	4.1	4.7	5.3	6.3	7.2	7.9	8.4
24	88 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	19.2	16.9	18.2	19.7	18.1	20.1	20.1	17.7	16.7	13.4	10.0	7.2	5.1	4.4	4.8	5.3	6.3	7.2	7.9	8.4
25	73 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	19.0	16.9	18.2	19.5	17.8	18.7	18.5	16.6	15.5	12.3	8.6	6.0	4.4	4.0	4.6	5.3	6.3	7.2	7.9	8.4
26	68 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	19.1	16.9	18.2	19.6	17.9	19.4	19.3	17.1	16.0	12.8	9.2	6.5	4.7	4.2	4.7	5.3	6.3	7.2	7.9	8.4
27	64 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	19.0	16.9	18.2	19.5	17.7	18.8	18.6	16.6	15.5	12.3	8.6	6.0	4.4	4.0	4.6	5.3	6.3	7.2	7.9	8.4
28	45 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.9	16.9	18.2	19.4	17.6	18.1	17.8	16.2	15.0	11.9	8.1	5.6	4.1	3.9	4.6	5.3	6.3	7.2	7.9	8.4
29	33 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.8	16.9	18.2	19.3	17.5	17.7	17.3	15.9	14.7	11.6	7.8	5.4	4.0	3.9	4.6	5.3	6.3	7.2	7.9	8.4
30	23 Fullam Hill Road	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.8	16.9	18.2	19.3	17.5	17.5	17.0	15.7	14.6	11.5	7.7	5.3	4.0	3.9	4.6	5.3	6.3	7.2	7.9	8.4
31	484 RT 119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.2	17.4	16.4	15.5	15.0	14.0	11.0	7.1	4.8	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
32	468 RT 119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.2	17.4	16.7	16.0	15.2	14.2	11.2	7.3	5.0	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
33	462 RT 119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.2	17.4	16.8	16.1	15.3	14.2	11.2	7.3	5.0	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
34	450 RT 119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.8	16.9	18.2	19.2	17.5	17.0	16.3	15.4	14.3	11.2	7.4	5.0	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
35	432 RT 119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.8	16.9	18.2	19.2	17.5	17.0	16.4	15.4	14.3	11.3	7.4	5.0	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
36	406 RT 1119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.8	16.9	18.2	19.2	17.4	17.2	16.6	15.5	14.4	11.3	7.5	5.1	3.9	3.9	4.6	5.3	6.3	7.2	7.9	8.4
37	377 RT 1119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.2	17.4	17.0	16.3	15.4	14.3	11.2	7.4	5.1	3.9	3.9	4.6	5.3	6.3	7.2	7.9	8.4
38	347 RT 1119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.1	17.3	16.4	15.6	15.0	14.0	11.0	7.1	4.8	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
39	334 RT 119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.9	16.9	18.2	19.3	17.5	17.9	17.5	16.1	16.0	12.9	9.5	7.1	5.2	4.6	4.9	5.4	6.3	7.2	7.9	8.4
40	327 RT 119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.2	17.4	16.9	16.2	15.4	14.2	11.2	7.5	5.2	4.0	3.9	4.7	5.3	6.3	7.2	7.9	8.4
41	328 RT 119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.8	16.9	18.2	19.2	17.5	17.4	16.9	15.7	14.5	11.5	7.8	5.4	4.1	4.0	4.7	5.3	6.3	7.2	7.9	8.4
42	310 RT 119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.2	17.4	16.7	16.0	15.2	14.1	11.1	7.3	5.0	3.9	3.9	4.6	5.3	6.3	7.2	7.9	8.4
43	269 RT 1119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.7	16.9	18.2	19.1	17.3	16.0	15.0	14.8	13.8	10.8	6.9	4.7	3.7	3.8	4.6	5.3	6.3	7.2	7.9	8.4
44	253 RT 1119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.6	16.9	18.2	19.1	17.3	15.8	14.8	14.7	13.9	10.9	7.0	4.8	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
45	224 RT 1119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.6	16.9	18.2	19.1	17.3	15.9	14.9	14.7	14.0	11.0	7.1	4.8	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
46	6 Phillips CT	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.6	16.9	18.2	19.1	17.3	15.7	14.7	14.6	13.9	10.9	7.0	4.8	3.7	3.8	4.6	5.3	6.3	7.2	7.9	8.4
47	14 Phillips CT	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.6	16.9	18.2	19.1	17.3	15.8	14.8	14.7	13.9	10.9	7.0	4.8	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4
48	206 RT 1119 E	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.6	16.9	18.2	19.0	17.3	15.7	14.7	14.6	13.9	10.9	6.9	4.7	3.7	3.8	4.6	5.3	6.3	7.2	7.9	8.4
49	15 Doyle CT	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.6	16.9	18.2	19.1	17.3	15.7	14.7	14.7	13.9	10.9	7.0	4.8	3.7	3.8	4.6	5.3	6.3	7.2	7.9	8.4
50	5 Doyle CT	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.6	16.9	18.2	19.0	17.2	15.7	14.6	14.6	13.8	10.8	6.9	4.7	3.7	3.8	4.6	5.3	6.3	7.2	7.9	8.4
51	18 Doyle CT	31.0	28.5	26.7	26.4	24.3	20.8	18.2	18.6	16.9	18.2	19.1	17.3	15.8	14.8	14.7	13.9	10.9	7.0	4.8	3.8	3.8	4.6	5.3	6.3	7.2	7.9	8.4

Nighttime Octave Band Analysis

Receptor ID	Address	Octave Band L90 (dB) from Source																										
		25.0	31.5	40.0	50.0	63.0	80.0	100	125	160	200	250	315	400	500	630	800	1000	1250	1600	2000	2500	3150	4000	5000	6300	8000	10000
1	10 Crane Road	-54.5	-46.2	-30.4	-39.1	-35.1	-25.5	-19	-3.2	-16.7	-14.1	-1.1	-2.5	5	5.1	0.8	-0.6	-4.9	-9	-14.2	-21.2	-29.6	-41.9	-60.9	-79.1	-80.3	-81.3	-82.7
2	3 Crane Road	-54.4	-46.2	-30.4	-39	-35.1	-25.5	-19	-3.2	-16.7	-14	-1.1	-2.5	5	5.1	0.9	-0.5	-4.8	-8.9	-14.2	-21.1	-29.4	-41.7	-60.6	-79.1	-80.3	-81.3	-82.7
3	19 Crane Road	-54	-45.7	-29.9	-38.5	-34.6	-25	-18.5	-2.6	-16.2	-13.5	-0.5	-1.9	5.6	5.8	1.5	0.1	-4.1	-8.1	-13.2	-19.9	-27.9	-39.6	-57.8	-78.2	-80.3	-81.3	-82.7
4	35 Crane Road	-53.3	-45	-29.2	-37.8	-33.9	-24.3	-17.7	-1.8	-15.3	-12.7	0.3	-1.1	6.5	6.7	2.5	1.2	-3	-6.8	-11.7	-18.1	-25.6	-36.5	-53.5	-75.3	-80.3	-81.3	-82.7
5	532 Rt 12 S	-55.4	-47.1	-31.3	-40	-36.1	-26.5	-20	-4.2	-17.8	-15.1	-2.2	-3.6	3.8	3.9	-0.4	-1.9	-6.4	-10.7	-16.2	-23.6	-32.7	-46.1	-66.7	-79.6	-80.3	-81.3	-82.7
6	549 Rt 12 S	-55.7	-47.4	-31.7	-40.3	-36.4	-26.8	-20.3	-4.5	-18.1	-15.5	-2.6	-4	3.4	3.5	-0.9	-2.4	-6.9	-11.3	-16.9	-24.5	-33.9	-47.7	-68.8	-79.7	-80.3	-81.3	-82.7
7	550 Rt 12 S	-56.4	-48.2	-32.4	-41	-37.1	-27.5	-21.1	-5.3	-18.9	-16.3	-3.5	-4.9	2.4	2.5	-1.9	-3.6	-8.2	-12.7	-18.6	-26.6	-36.6	-51.4	-73.3	-79.7	-80.3	-81.3	-82.7
8	444 Fullam Hill Road	-57.8	-49.6	-33.8	-42.5	-38.5	-29	-22.6	-6.8	-20.5	-17.9	-5.2	-6.7	0.6	0.5	-4	-5.8	-10.7	-15.6	-22	-30.9	-42.4	-59.4	-78.4	-79.7	-80.3	-81.3	-82.7
9	423 Fullam Hill Road	-57.9	-49.7	-33.9	-42.6	-38.6	-29.1	-22.7	-6.9	-20.6	-18.1	-5.3	-6.8	0.4	0.3	-4.2	-6	-10.9	-15.8	-22.3	-31.2	-42.8	-60	-78.5	-79.7	-80.3	-81.3	-82.7
10	414 Fullam Hill Road	-57	-48.7	-32.9	-41.6	-37.7	-28.1	-21.6	-5.9	-19.5	-16.9	-4.1	-5.6	1.7	1.7	-2.7	-4.4	-9.1	-13.8	-19.9	-28.2	-38.7	-54.4	-76	-79.7	-80.3	-81.3	-82.7
11	391 Fullam Hill Road	-57	-48.7	-33	-41.6	-37.7	-28.1	-21.7	-5.9	-19.6	-17	-4.1	-5.7	1.7	1.7	-2.8	-4.5	-9.2	-13.8	-20	-28.3	-38.9	-54.6	-76.1	-79.7	-80.3	-81.3	-82.7
12	364 Fullam Hill Road	-55.8	-47.6	-31.8	-40.4	-36.5	-26.9	-20.4	-4.7	-18.2	-15.6	-2.7	-4.2	3.2	3.3	-1.1	-2.6	-7.1	-11.5	-17.2	-24.8	-34.3	-48.3	-69.6	-79.7	-80.3	-81.3	-82.7
13	309 Fullam Hill Road	-54.1	-45.8	-30	-38.6	-34.7	-25.1	-18.6	-2.7	-16.3	-13.6	-0.7	-2	5.5	5.6	1.4	0	-4.3	-8.3	-13.4	-20.1	-28.2	-40	-58.4	-78.4	-80.3	-81.3	-82.7
14	307 Fullam Hill Road	-53.6	-45.3	-29.6	-38.2	-34.3	-24.6	-18.1	-2.3	-15.8	-13.1	-0.2	-1.5	6	6.2	2	0.6	-3.6	-7.5	-12.5	-19.1	-26.9	-38.2	-55.8	-77.2	-80.3	-81.3	-82.7
15	277 Fullam Hill Road	-52.2	-43.9	-28.1	-36.8	-32.8	-23.2	-16.4	-0.6	-14.1	-11.6	1.5	0.2	7.7	8	3.8	2.4	-1.7	-5.4	-10.1	-16.2	-23.2	-33.3	-48.8	-70	-80.3	-81.3	-82.7
16	264 Fullam Hill Road	-51.6	-43.3	-27.5	-36.2	-32.2	-22.6	-15.7	0.2	-13.3	-10.9	2.2	0.9	8.5	8.7	4.6	3	-1.1	-4.8	-9.5	-15.4	-22.2	-31.9	-46.8	-67	-80.2	-81.3	-82.7
17	199 Fullam Hill Road	-47.4	-39.1	-23.4	-32	-28	-18.3	-10	5.9	-7.5	-6.5	6.6	5.5	13.2	13.6	9.6	8.9	5.2	2.2	-1.5	-6	-10.7	-17.1	-27.1	-40.2	-58	-79.6	-82.7
18	161 Fullam Hill Road	-44.3	-36.1	-20.3	-28.9	-24.9	-15.2	-6.9	9.1	-4.3	-3.3	9.9	8.8	16.5	17	13.1	12.4	8.9	6	2.6	-1.5	-5.3	-10.6	-18.6	-28.7	-41.9	-61.2	-81.8
19	123 Fullam Hill Road	-43.8	-35.6	-19.8	-28.4	-24.4	-14.7	-6.4	9.6	-3.8	-2.8	10.4	9.3	17	17.5	13.6	12.9	9.3	6.4	3.1	-1	-4.8	-9.9	-17.8	-27.5	-40.2	-58.8	-80.8
20	106 Fullam Hill Road	-42.2	-33.9	-18.1	-26.7	-22.7	-13	-4.7	11.3	-2.1	-1.1	12.1	11	18.8	19.3	15.4	14.7	11.3	8.4	5.2	1.4	-2.1	-6.7	-13.7	-22.2	-33	-48.7	-70.8
21	99 Fullam Hill Road	-44.6	-36.4	-20.6	-29.2	-25.2	-15.5	-7.2	8.8	-4.6	-3.6	9.6	8.5	16.2	16.7	12.8	12	8.4	5.5	2	-2.1	-6.1	-11.5	-19.9	-30.3	-44	-64.2	-82.3
22	94 Fullam Hill Road	-43.5	-35.2	-19.4	-28	-24	-14.3	-6	10	-3.4	-2.4	10.8	9.7	17.4	17.9	14	13.3	9.8	7	3.7	-0.3	-4	-8.9	-16.5	-25.9	-38	-55.7	-78.9
23	85 Fullam Hill Road	-45.7	-37.4	-21.6	-30.2	-26.3	-16.6	-8.2	7.7	-5.7	-4.7	8.5	7.3	15.1	15.5	11.6	10.7	7.1	4.1	0.6	-3.7	-8	-13.8	-22.8	-34.2	-49.5	-71.6	-82.7
24	88 Fullam Hill Road	-44.5	-36.2	-20.4	-29	-25	-15.3	-7	9	-4.4	-3.4	9.7	8.6	16.4	16.8	12.9	12.3	8.8	5.9	2.5	-1.5	-5.3	-10.5	-18.5	-28.6	-41.8	-61.1	-81.8
25	73 Fullam Hill Road	-46.7	-38.4	-22.6	-31.2	-27.2	-17.6	-9.2	6.7	-6.7	-5.7	7.4	6.3	14	14.4	10.5	9.6	5.9	2.8	-0.8	-5.3	-9.9	-16.1	-25.8	-38.4	-55.3	-77.8	-82.7
26	68 Fullam Hill Road	-46	-37.7	-21.9	-30.6	-26.6	-16.9	-8.6	7.4	-6	-5	8.1	7	14.7	15.1	11.2	10.4	6.8	3.8	0.2	-4.1	-8.5	-14.4	-23.5	-35.3	-51	-73.4	-82.7
27	64 Fullam Hill Road	-47.5	-39.2	-23.4	-32.1	-28.1	-18.4	-10.1	5.8	-7.6	-6.6	6.6	5.4	13.1	13.5	9.5	8.6	4.9	1.7	-2.1	-6.7	-11.6	-18.3	-28.6	-42.2	-60.6	-80.5	-82.7
28	45 Fullam Hill Road	-49	-40.7	-24.9	-33.6	-29.6	-19.9	-12	3.9	-9.5	-8.1	5	3.8	11.4	11.8	7.8	6.8	3	-0.3	-4.4	-9.4	-14.7	-22.3	-33.9	-49.5	-70.7	-81.3	-82.7
29	33 Fullam Hill Road	-50.1	-41.9	-26.1	-34.7	-30.7	-21.1	-13.7	2.2	-11.3	-9.3	3.7	2.5	10.1	10.5	6.4	5.3	1.4	-2	-6.2	-11.5	-17.3	-25.6	-38.5	-55.9	-77.3	-81.3	-82.7
30	23 Fullam Hill Road	-50.9	-42.6	-26.8	-35.4	-31.5	-21.8	-14.7	1.2	-12.3	-10.1	3	1.7	9.3	9.6	5.5	4.4	0.5	-3.1	-7.4	-12.9	-19.1	-27.9	-41.6	-60.3	-79.4	-81.3	-82.7
31	484 RT 119 E	-51.3	-43	-27.2	-35.9	-31.9	-22.3	-15.3	0.6	-12.9	-10.6	2.5	1.2	8.8	9.1	5	3.3	-0.7	-4.5	-9.1	-15	-21.6	-31	-45.6	-65.4	-80.1	-81.3	-82.7
32	468 RT 119 E	-50.5	-42.2	-26.4	-35.1	-31.1	-21.5	-14.2	1.7	-11.8	-9.8	3.3	2.1	9.7	10	6	4.8	0.9	-2.5	-6.8	-12.2	-18.3	-26.8	-40.1	-58.2	-78.7	-81.3	-82.7
33	462 RT 119 E	-50.3	-42	-26.2	-34.9	-30.9	-21.3	-13.9	1.9	-11.5	-9.5	3.6	2.3	9.9	10.3	6.2	5.1	1.2	-2.2	-6.5	-11.8	-17.8	-26.2	-39.2	-57	-78	-81.3	-82.7
34	450 RT 119 E	-50.3	-42	-26.3	-34.9	-30.9	-21.3	-14	1.9	-11.5	-9.6	3.5	2.3	9.9	10.2	6.2	5.1	1.2	-2.3	-6.5	-11.9	-17.8	-26.2	-39.3	-57.1	-78.1	-81.3	-82.7
35	432 RT 119 E	-50.7	-42.4	-26.6	-35.3	-31.3	-21.7	-14.5	1.4	-12.1	-10	3.1	1.9	9.5	9.8	5.7	4.6	0.7	-2.8	-7.2	-12.6	-18.8	-27.5	-41	-59.4	-79.2	-81.3	-82.7
36	406 RT 1119 E	-51.5	-43.2	-27.4	-36	-32.1	-22.4	-15.5	0.3	-13.1	-10.8	2.3	1	8.6	8.9	4.8	3.6	-0.4	-4	-8.5	-14.2	-20.7	-30	-44.5	-64.3	-80.1	-81.3	-82.7
37	377 RT 1119 E	-52.8	-44.5	-28.8	-37.4	-33.5	-23.8	-17.2	-1.3	-14.8	-12.3	0.8	-0.6	7	7.2	3	1.7	-2.4	-6.2	-11	-17.3	-24.6	-35.1	-51.5	-73.3	-80.3	-81.3	-82.7
38	347 RT 1119 E	-54.5	-46.2	-30.5	-39.1	-35.2	-25.6	-19	-3.2	-16.8	-14.1	-1.2	-2.5	4.9	5.1	0.8	-0.8	-5.2	-9.4	-14.7	-21.8	-30.3	-42.8	-62	-79.3	-80.3	-81.3	-82.7
39	334 RT 119 E	-53.9	-45.6	-29.9	-38.5	-34.6	-24.9	-18.4	-2.6	-16.1	-13.5	-0.5	-1.9	5.6	5.8	1.6	0.2	-4	-8	-13.1	-19.8	-27.8	-39.5	-57.5	-78.1	-80.3	-81.3	-82.7
40	327 RT 119 E	-54.8	-46.5	-30.7	-39.4	-35.5	-25.9	-19.3	-3.5	-17	-14.4	-1.4	-2.8	4.6	4.8	0.5	-1.9	-6.5	-10.9	-16.5	-23.9	-32.9	-46	-65.9	-79.6	-80.3	-81.3	-82.7
41	328 RT 119 E	-54.8	-46.5	-30.7	-39.4	-35.4	-25.8	-19.3	-3.5	-17.1	-14.4	-1.5	-2.9	4.6	4.7	0.4	-1.2	-5.6	-9.8	-15.2	-22.4	-31.1	-43.8	-63.5	-79.5	-80.3	-81.3	-82.7
42	310 RT 119 E	-55.4	-47.1	-31.3	-40	-36.1	-26.5	-20	-4.2	-17.7	-15.1	-2.2	-3.6	3.8	3.9	-0.4	-2.1	-6.6	-11	-16.6	-24	-33.2	-46.8	-67.5	-79.7	-80.3	-81.3	-82.7
43	269 RT 1119 E	-56.9	-48.7	-32.9	-41.5	-37.6	-28	-21.6	-5.9	-19.5	-16.9	-4.1	-5.6	1.8	1.8	-2.7	-4.4	-9	-13.7	-19.8	-28.1	-38.6	-54.2	-75.8	-79.7	-80.3	-81.3	-82.7
44	253 RT 1119 E	-57.5	-49.2	-33.4	-42.1	-38.2	-28.6	-22.2	-6.4	-20.1	-17.5	-4.7	-6.2	1.1	1	-3.5	-5.2	-10	-14.8	-21.1	-29.7	-40.8	-57.2	-77.6	-79.7	-80.3	-81.3	-82.7
45	224 RT 1119 E	-57.6	-49.3	-33.5	-42.2	-38.3	-28.7	-22.3	-6.5	-20.2	-17.6	-4.8	-6.3	0.9	0.9	-3.6	-5.4	-10.2	-15	-21.3	-30	-41.1	-57.7	-77.9	-79.7	-80.3	-81.3	-82.7
46	6 Phillips CT	-58.1	-49.8	-34	-42.7	-38.8	-29.2	-22.8	-7.1	-20.8	-18.2	-5.4	-7	0.2	0.1	-4.4	-6.2	-11.1	-16.1	-22.7	-31.7	-43.4	-60.8	-78.7	-79.7	-80.3	-81.3	-82.7
47	14 Phillips CT	-57.8	-49.5	-33.8	-42.4	-38.5	-28.9	-22.5	-6.8	-20.4	-17.9	-5.1	-6.7	0.6	0.6	-4	-5.8	-10.6	-15.5	-21.9	-30.8	-42.2	-59.1	-78.3	-79.7	-80.3	-81.3	-82.7
48	206 RT 1119 E	-58.2	-49.9	-34.2	-42.8	-38.9	-29.4	-22.9	-7.2	-20.9	-18.4	-5.6	-7.2	0.1	0	-4.6	-6.4	-11.3	-16.3	-23	-32.1	-43.9	-61.6	-78.8	-79.7	-80.3	-81.3	-82.7
49	15 Doyle CT	-58	-49.7	-34	-42.6	-38.7	-29.2	-22.7	-7	-20.7	-18.2	-5.4	-6.9	0.3	0.2	-4.3	-6.1	-11	-15.9	-22.5	-31.5	-43.1	-60.4	-78.6	-79.7	-80.3	-81.3	-82.7
50	5 Doyle CT	-58.3	-50.1	-34.3	-43	-39.1	-29.5	-23.1	-7.4	-21.1	-18.5	-5.8	-7.4	-0.1	-0.3	-4.8	-6.7	-11.6	-16.7	-23.4	-32.6	-44.6	-62.5	-78.9	-79.7	-80.3	-81.3	-82.7
51	18 Doyle CT	-57.9	-49.6	-33.8	-42.5	-38.6	-29	-22.6	-6.9	-20.5	-18	-5.2	-6.7	0.5	0.5	-4.1	-5.9	-10.7	-15.6	-22.1	-31	-42.5	-59.5	-78.4	-79.7	-80.3	-81.3	-82.7

	Octave Band L90 (dB) from Background																											
	25.0	31.5	40.0	50.0	63.0	80.0	100	125	160	200	250	315	400	500	630	800	1000	1250	1600	2000	2500	3150	4000	5000	6300	8000	10000
Lowest Nightime L90	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.5	8.5	11.5	11.4	11	10.2	10.7	11.8	10.5	8.4	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4

Receptor ID	Address	Octave Band L90 (dB) from Source& Background																										
		25.0	31.5	40.0	50.0	63.0	80.0	100	125	160	200	250	315	400	500	630	800	1000	1250	1600	2000	2500	3150	4000	5000	6300	8000	10000
1	10 Crane Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.7	8.5	11.5	11.6	11.2	11.3	11.8	12.1	10.8	8.6	6.9	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
2	3 Crane Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.7	8.5	11.5	11.6	11.2	11.3	11.8	12.1	10.8	8.6	6.9	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
3	19 Crane Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.8	8.5	11.5	11.7	11.2	11.5	11.9	12.2	10.9	8.6	6.9	6.2	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
4	35 Crane Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.8	8.5	11.5	11.7	11.3	11.7	12.2	12.3	11.0	8.7	7.0	6.2	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
5	532 Rt 12 S	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.7	8.5	11.5	11.6	11.1	11.1	11.5	12.1	10.7	8.5	6.9	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
6	549 Rt 12 S	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.7	8.5	11.5	11.6	11.1	11.0	11.5	12.0	10.7	8.5	6.9	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
7	550 Rt 12 S	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.9	11.3	12.0	10.7	8.5	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
8	444 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.7	11.1	11.9	10.6	8.5	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
9	423 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.6	11.1	11.9	10.6	8.5	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
10	414 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.8	11.2	12.0	10.6	8.5	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
11	391 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.8	11.2	11.9	10.6	8.5	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
12	364 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.7	8.5	11.5	11.6	11.1	11.0	11.4	12.0	10.7	8.5	6.9	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
13	309 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.8	8.5	11.5	11.7	11.2	11.5	11.9	12.2	10.9	8.6	6.9	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
14	307 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.8	8.5	11.5	11.7	11.2	11.6	12.0	12.2	10.9	8.7	7.0	6.2	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
15	277 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.9	8.5	11.5	11.8	11.3	12.1	12.6	12.4	11.1	8.8	7.1	6.2	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
16	264 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	10.0	8.5	11.5	11.9	11.4	12.4	12.8	12.6	11.2	8.9	7.1	6.2	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
17	199 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	11.1	8.6	11.6	12.6	12.1	15.0	15.4	13.8	12.8	10.1	8.1	6.8	4.8	4.2	4.5	5.2	6.2	7.1	7.8	8.4
18	161 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.3	12.3	8.7	11.6	13.7	13.0	17.4	17.9	15.5	14.6	11.7	9.4	7.7	5.4	4.6	4.6	5.2	6.2	7.1	7.8	8.4
19	123 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.3	12.6	8.7	11.7	13.9	13.2	17.8	18.3	15.8	14.9	11.9	9.6	7.9	5.5	4.6	4.7	5.2	6.2	7.1	7.8	8.4
20	106 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.3	13.5	8.9	11.7	14.8	14.0	19.4	19.9	17.0	16.1	13.1	10.7	8.7	6.2	5.0	4.8	5.3	6.2	7.1	7.8	8.4
21	99 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.3	12.2	8.7	11.6	13.6	12.9	17.2	17.7	15.3	14.3	11.4	9.2	7.5	5.3	4.5	4.6	5.2	6.2	7.1	7.8	8.4
22	94 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.3	12.8	8.8	11.7	14.1	13.4	18.2	18.7	16.0	15.1	12.2	9.9	8.1	5.7	4.7	4.7	5.2	6.2	7.1	7.8	8.4
23	85 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	11.7	8.7	11.6	13.2	12.5	16.3	16.7	14.7	13.6	10.8	8.7	7.2	5.0	4.4	4.6	5.2	6.2	7.1	7.8	8.4
24	88 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.3	12.3	8.7	11.6	13.6	13.0	17.3	17.8	15.4	14.5	11.6	9.4	7.7	5.4	4.6	4.6	5.2	6.2	7.1	7.8	8.4
25	73 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	11.3	8.6	11.6	12.9	12.3	15.5	15.9	14.2	13.1	10.3	8.3	6.9	4.8	4.3	4.5	5.2	6.2	7.1	7.8	8.4
26	68 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	11.6	8.7	11.6	13.1	12.5	16.0	16.4	14.5	13.5	10.7	8.6	7.1	5.0	4.3	4.6	5.2	6.2	7.1	7.8	8.4
27	64 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	11.0	8.6	11.6	12.6	12.1	14.9	15.3	13.8	12.7	10.0	8.0	6.7	4.7	4.2	4.5	5.2	6.2	7.1	7.8	8.4
28	45 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	10.6	8.6	11.5	12.3	11.8	13.9	14.3	13.3	12.0	9.5	7.6	6.5	4.6	4.2	4.5	5.2	6.2	7.1	7.8	8.4
29	33 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	10.2	8.5	11.5	12.1	11.6	13.2	13.6	12.9	11.6	9.2	7.3	6.3	4.5	4.1	4.5	5.2	6.2	7.1	7.8	8.4
30	23 Fullam Hill Road	26.3	22.8	20.6	18.9	16.7	12.9	11.2	10.1	8.5	11.5	12.0	11.5	12.8	13.2	12.7	11.5	9.1	7.2	6.3	4.5	4.1	4.5	5.2	6.2	7.1	7.8	8.4
31	484 RT 119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	10.0	8.5	11.5	11.9	11.4	12.6	13.0	12.6	11.3	8.9	7.1	6.2	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
32	468 RT 119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	10.2	8.5	11.5	12.0	11.5	13.0	13.4	12.8	11.5	9.1	7.3	6.3	4.5	4.1	4.5	5.2	6.2	7.1	7.8	8.4
33	462 RT 119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	10.2	8.5	11.5	12.1	11.5	13.1	13.5	12.9	11.6	9.2	7.3	6.3	4.5	4.1	4.5	5.2	6.2	7.1	7.8	8.4
34	450 RT 119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	10.2	8.5	11.5	12.1	11.5	13.1	13.5	12.9	11.6	9.2	7.3	6.3	4.5	4.1	4.5	5.2	6.2	7.1	7.8	8.4
35	432 RT 119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	10.1	8.5	11.5	12.0	11.5	12.9	13.3	12.8	11.5	9.1	7.3	6.3	4.5	4.1	4.5	5.2	6.2	7.1	7.8	8.4
36	406 RT 1119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	10.0	8.5	11.5	11.9	11.4	12.5	12.9	12.6	11.3	8.9	7.1	6.2	4.5	4.1	4.5	5.2	6.2	7.1	7.8	8.4
37	377 RT 1119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.8	8.5	11.5	11.8	11.3	11.9	12.3	12.3	11.0	8.7	7.0	6.2	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
38	347 RT 1119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.7	8.5	11.5	11.6	11.2	11.3	11.8	12.1	10.8	8.6	6.9	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
39	334 RT 119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.8	8.5	11.5	11.7	11.2	11.5	11.9	12.2	10.9	8.6	6.9	6.2	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
40	327 RT 119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.7	8.5	11.5	11.6	11.2	11.3	11.7	12.1	10.7	8.5	6.9	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
41	328 RT 119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.7	8.5	11.5	11.6	11.2	11.3	11.7	12.1	10.8	8.6	6.9	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
42	310 RT 119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.7	8.5	11.5	11.6	11.1	11.1	11.5	12.1	10.7	8.5	6.9	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
43	269 RT 1119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.8	11.2	12.0	10.6	8.5	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
44	253 RT 1119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.7	11.1	11.9	10.6	8.5	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
45	224 RT 1119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.7	11.1	11.9	10.6	8.5	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
46	6 Phillips CT	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.6	11.1	11.9	10.6	8.4	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
47	14 Phillips CT	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.7	11.1	11.9	10.6	8.5	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
48	206 RT 1119 E	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.6	11.1	11.9	10.6	8.4	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
49	15 Doyle CT	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.6	11.1	11.9	10.6	8.4	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
50	5 Doyle CT	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.6	11.0	11.9	10.6	8.4	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4
51	18 Doyle CT	26.3	22.8	20.6	18.9	16.7	12.9	11.2	9.6	8.5	11.5	11.5	11.1	10.6	11.1	11.9	10.6	8.5	6.8	6.1	4.4	4.1	4.5	5.2	6.2	7.1	7.8	8.4